## SYMMETRY-FORCED FORMATION CONTROL

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#### **FORMATION CONTROL**







# **Formation Control Objective**

Given a team of robots endowed with the ability to sense/ communicate with neighboring robots, design a control for each robot using only local information that moves the team into a desired spatial configuration.

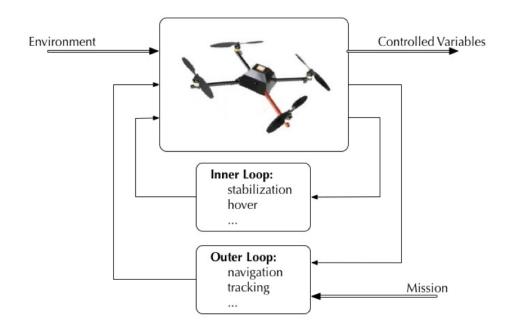




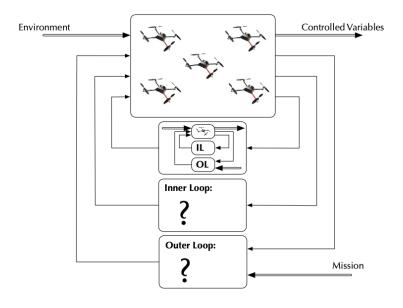


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### **CONTROL ARCHITECTURES**



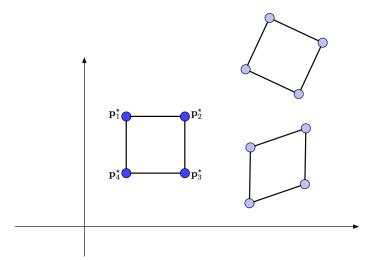
# **CONTROL ARCHITECTURES FOR MULTI-AGENT SYSTEMS**



#### **FORMATION CONSTRAINTS**

- The desired formation is characterized by a set of M constraints, encoded in the function  $F: \mathbb{R}^{nd} \to \mathbb{R}^M$ , and a configuration  $\mathbf{p}^*$  satisfying the constraints.
- The set of all feasible formations is

$$\mathcal{F}(p) = \{ p \in \bar{\mathcal{D}} \,|\, F(p) = F(\mathbf{p}^*) \}$$



### **FORMATION CONTROL PROBLEM**

# **Formation Control Objective**

For an ensemble of n agents with dynamics

$$\dot{p}_i = u_i,$$

with  $p_i(t) \in \mathbb{R}^d$ , an information exchange graph  $\mathcal{G} = (\mathcal{V}, \mathcal{E})$ , and formation constraint function  $F : \mathbb{R}^{nd} \to \mathbb{R}^M$ , design a distributed control law for each agent  $i \in \{1, \dots, n\}$  such that the set  $\mathcal{F}(p) = \{p \in \bar{\mathcal{D}} \mid F(p) = F(\mathbf{p}^*)\},$ 

is asymptotically stable.

### **Theorem - Distance Constrained Formation Control**

[Krick 2009]

Consider the potential function

$$F_f(p) = \frac{1}{4} \sum_{ij \in \mathcal{E}} (\|p_i(t) - p_j(t)\|^2 - \mathbf{d}_{ij}^2)^2$$

and assume the desired distances  $\mathbf{d}_{ij}$  correspond to a feasible formation. Then the gradient dynamical system

$$u_i = -\nabla_{p_i} F_f(p) = \sum_{ij \in \mathcal{E}} (\|p_i - p_j\|^2 - \mathbf{d}_{ij}^2) (p_j - p_i)$$

asymptotically converges to the critical points of the potential function, i.e.,  $\frac{\partial F_f(p)}{\partial p}=0$ .

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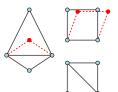
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- · ensures convergence to correct edge lengths!
- · ...but how do we ensure the correct shape?



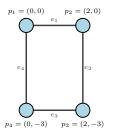
#### A NOTE ON FORMATION POTENTIALS AND RIGIDITY THEORY

$$F_f(p) = \frac{1}{4} \sum_{ij \in \mathcal{E}} (\|p_i(t) - p_j(t)\|^2 - \mathbf{d}_{ij}^*)^2)^2$$

formation potential can be written in terms of a rigidity function

$$F_f(p) = \frac{1}{2} ||r_{\mathcal{G}}(p) - r_{\mathcal{G}}(\mathbf{p})||^2$$

- $\begin{bmatrix} F_f(p) = \frac{1}{2} \|r_{\mathcal{G}}(p) r_{\mathcal{G}}(\mathbf{p})\|^2 \\ \\ \circ \ r_{\mathcal{G}} : p \mapsto \begin{bmatrix} \cdots & \frac{1}{2} \|p_i p_j\|^2 & \cdots \end{bmatrix}^T \text{: distances between neighbors} \end{cases}$
- $\circ \ \mathbf{p}$ : a configuration satisfying distance constraints (i.e.,  $\|\mathbf{p}_i \mathbf{p}_i\|^2 = \mathbf{d}_{ii}^2$ )



$$r_{\mathcal{G}}(p) = \begin{bmatrix} \|p_1 - p_2\|^2 \\ \|p_2 - p_3\|^2 \\ \|p_3 - p_4\|^2 \\ \|p_4 - p_1\|^2 \end{bmatrix} = \begin{bmatrix} 4 \\ 9 \\ 4 \\ 9 \end{bmatrix}$$

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- $\left[ F_f(p) = \frac{1}{2} \| r_{\mathcal{G}}(p) r_{\mathcal{G}}(\mathbf{p}) \|^2 \right]$   $\circ \ r_{\mathcal{G}} : p \mapsto \left[ \cdots \quad \frac{1}{2} \| p_i p_j \|^2 \quad \cdots \right]^T \text{: distances between neighbors}$
- $\circ \ \mathbf{p}$ : a configuration satisfying distance constraints (i.e.,  $\|\mathbf{p}_i \mathbf{p}_j\|^2 = \mathbf{d}_{ij}^2$ )
- rigidity theory looks for distance-preserving infinitesimal motions

$$r_{\mathcal{G}}(p+\delta p) = r_{\mathcal{G}}(p) + \frac{\partial r_{\mathcal{G}}(p)}{\partial p} \delta p + \text{h.o.t}$$

- $\circ$  infinitesimal motions satisfy  $\frac{\partial r_{\mathcal{G}}(p)}{\partial n}\delta p=0$
- the Rigidity matrix :  $R(p) = \frac{\partial r_{\mathcal{G}}(p)}{\partial x} \in \mathbb{R}^{|\mathcal{E}| \times 2|\mathcal{V}|}$
- o "rigid body" rotations and translations are always distance preserving: trivial motions
- $\circ$  A framework  $(\mathcal{G}, p)$  is infinitesimally rigid if the only infinitesimal motions are trivial

### our formation control

$$u_i = -\nabla_{p_i} F_f(p) = \sum_{ij \in \mathcal{E}} (\|p_i - p_j\|^2 - \mathbf{d}_{ij}^2) (p_j - p_i)$$

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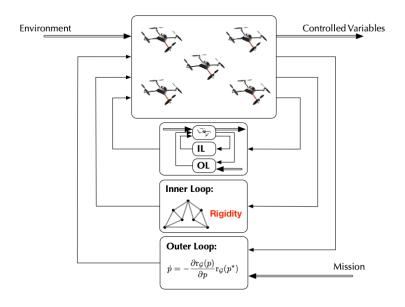
a proof sketch

• define error dynamics for distance error:  $e = R(p)p - d^2$ 

$$\dot{e} = -R(p)R^T(p)e$$

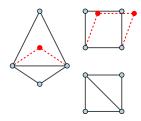
- Lyapunov argument  $V(e) = \frac{1}{2} \|e\|^2$ 
  - when  $R(p)R^{T}(p) > 0$ , we have (local) exponential convergence to desired formation
  - good frameworks are i) infinitesimally rigid, and ii) full row-rank (isostatic farmeworks)

# **CONTROL ARCHITECTURES FOR MULTI-AGENT SYSTEMS**



# Rigidity theory helps us understand

- how many constraints are required to ensure uniqueness of formation shape (modulo translations, rotations, and flip ambiguities)
- how the constraints should be distributed in the network

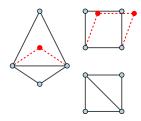


A widely accepted architectural requirement for distance constrained formation control is that isostatic frameworks are required. Equivalent to:

$$\operatorname{rk} R(p) = 2|\mathcal{V}| - 3$$
 and  $|\mathcal{E}| = 2|\mathcal{V}| - 3$  (in  $\mathbb{R}^2$ )

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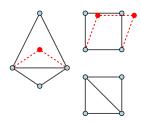
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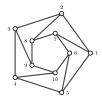


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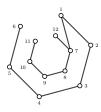
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**A:** Impose additional symmetry constraints without requiring more information exchange (in fact, less!)



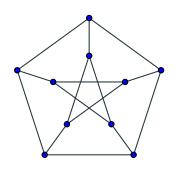
 The "classic" distance based formation control strategy requires at least 21 edges



 Incorporating (rotational) symmetry constraints lowers the number of required edges to 11

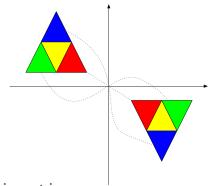
### **GRAPH SYMMETRIES AND POINT GROUPS**

# **Graph Symmetries**



• graph automorphisms

# **Point Groups**



isometries

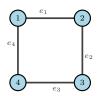
#### SYMMETRY AND GRAPH AUTOMORPHISMS

# Automorphisms encode graph symmetries

# **Graph Automorphism**

An automorphism of the graph  $\mathcal{G} = (\mathcal{V}, \mathcal{E})$  is a permutation  $\psi : \mathcal{V} \to \mathcal{V}$  of its vertex set such that

$$\{v_i, v_j\} \in \mathcal{E} \Leftrightarrow \{\psi(v_i), \psi(v_j)\} \in \mathcal{E}$$



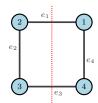
Identity:

$$Id = \begin{pmatrix} 1 & 2 & 3 & 4 \\ 1 & 2 & 3 & 4 \end{pmatrix}$$



clock-wise  $90^{\circ}$  rotation:

$$\psi_1 = \left( \begin{array}{cccc} 1 & 2 & 3 & 4 \\ 2 & 3 & 4 & 1 \end{array} \right)$$

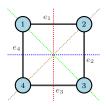


reflection:

$$Id = \begin{pmatrix} 1 & 2 & 3 & 4 \\ 1 & 2 & 3 & 4 \end{pmatrix} \qquad \psi_1 = \begin{pmatrix} 1 & 2 & 3 & 4 \\ 2 & 3 & 4 & 1 \end{pmatrix} \qquad \psi_2 = \begin{pmatrix} 1 & 2 & 3 & 4 \\ 2 & 1 & 4 & 3 \end{pmatrix}$$

### **AUTOMORPHISM GROUPS**

 Additional permutations can be found for the given graph considering all possible reflections and rotations



- The set of all automorphisms of  $\mathcal{G}$  form a group  $\operatorname{Aut}(\mathcal{G})$ 
  - Aut( $\mathcal{G}$ ) = {Id,  $\psi_1, \psi_2, ...$ }
- A subgroup is a subset of a group, and also satisfies all properties of a group
  - $\{\mathrm{Id}, \psi_1, \psi_2, \psi_3\}$
  - $\{\mathrm{Id}, \psi_2, \psi_4, \psi_5\}$
  - $\{ \mathrm{Id}, \psi_2 \}$
  - $\{ \mathrm{Id}, \psi_6 \}$
  - $\{ \mathrm{Id}, \psi_7 \}$
- For any subgroup  $\Gamma \subseteq \operatorname{Aut}(\mathcal{G})$ , we say that  $\mathcal{G}$  is  $\Gamma$ -symmetric, which define specific symmetries in  $\mathcal{G}$

### $\Gamma$ -SYMMETRIC FRAMEWORKS

## **Definition**

For a  $\Gamma$ -symmetric graph  $\mathcal{G}=(\mathcal{V},\mathcal{E})$  and vertex  $i\in\mathcal{V}$ , the set  $\Gamma_i=\{\gamma(i)\,|\,\gamma\in\Gamma\}$  is called the vertex orbit of i. Similarly, for an edge  $e=ij\in\mathcal{E}$ , the set  $\Gamma_e=\{\gamma(i)\gamma(j)\,|\,\gamma\in\Gamma\}$  is termed the edge orbit of e.





consider  $\Gamma = \{ \mathrm{Id}, \psi_2 \}$  (reflection about mirror S)

· Vertex Orbit:

$$\Gamma_1 = \Gamma_2 = \{1, 2\}, \ \Gamma_3 = \Gamma_4 = \{3, 4\}$$

• Edge Orbit:

$$\Gamma_{e_1} = \{e_1\}, \ \Gamma_{e_3} = \{e_3\}, \ \Gamma_{e_2} = \Gamma_{e_4} = \{e_2, e_4\}$$

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 vertices inside a vertex orbit are equivalent representative vertex set:  $\mathcal{V}_0 = \{1, 4\}$ 

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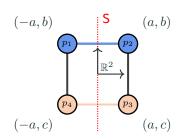
# $au(\Gamma)$ -symmetric frameworks

Let  $\Gamma$  be represented as a point group.

- homomorphism  $\tau:\Gamma\to O(\mathbb{R}^d)$
- au assigns an orthogonal matrix (describing an isometry of  $\mathbb{R}^d$ ) to each element of  $\Gamma$

### **Definition**

A framework  $(\mathcal{G}, p)$  in  $\mathbb{R}^d$  is called  $\tau(\Gamma)$ -symmetric if  $\tau(\gamma)(p_i) = p_{\gamma(i)} \quad \text{for all } \gamma \in \Gamma \text{ and all } i \in \mathcal{V}.$ 



• Consider  $\Gamma = \{ \mathrm{Id}, \psi_2 \}$  (Reflection about mirror S)

• Isometry 
$$au(\psi_2)= au_s=egin{bmatrix} -1 & 0 \\ 0 & 1 \end{bmatrix}$$
: 
$$au_sp_1=egin{bmatrix} -1 & 0 \\ 0 & 1 \end{bmatrix} egin{bmatrix} -a \\ b \end{bmatrix} = egin{bmatrix} a \\ b \end{bmatrix} = p_2$$
 
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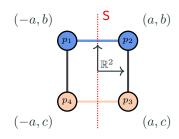
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- isometries of the desired configuration coincide with symmetries of the automorphisms of  ${\cal G}$
- symmetries can lead to unexpected infinitesimal flexibility/rigidity

#### SYMMETRIC RIGIDITY

## **Definition**

An infinitesimal motion u of a  $\tau(\Gamma)$ -symmetric framework  $(\mathcal{G},p)$  is  $\tau(\Gamma)$ -symmetric if

$$\tau(\gamma)(u_i) = u_{\gamma(i)}$$
 for all  $\gamma \in \Gamma$  and all  $i \in \mathcal{V}$ .

We say that  $(\mathcal{G}, p)$  is  $\tau(\Gamma)$ -symmetric infinitesimally rigid if every  $\tau(\Gamma)$ -symmetric infinitesimal motion is trivial.

- recall that infinitesimal motions are in the kernel of the rigidity matrix

$$R(p)\delta p = 0$$

- we can find a subspace of the kernel that is isomorphic to the space of 'fully-symmetric' infinitesimal motions
- velocity assignments to the points of  $(\mathcal{G},p)$  that exhibit exactly the same symmetry as the configuration p

# **Symmetric Formation Control Objective**

Consider a group of n integrator agents that interact over the  $\Gamma$ -symmetric sensing graph  $\mathcal{G}$ . Let  $\mathbf{p} \in \mathbb{R}^{dn}$  be a configuration such that  $(\mathcal{G}, \mathbf{p})$  is  $\tau(\Gamma)$ -symmetric for some desired point group  $\tau(\Gamma)$ , and let  $\mathcal{V}_0$  be a set of representatives of the vertex orbits of  $\mathcal{G}$  under  $\Gamma$ . Design a control  $u_i(t)$  for each agent i such that

(i) 
$$\lim_{t\to\infty} \|p_i(t) - p_j(t)\| = \|\mathbf{p}_i - \mathbf{p}_j\| = \mathbf{d}_{ij}$$
 for all  $ij \in \mathcal{E}$ ; (distance constraints)

(ii) 
$$\lim_{t\to\infty} \|p_u(t) - \tau(\gamma_{vu})p_v(t)\| = 0$$
 for all  $u, v \in \Gamma_i$ ,  $i \in \mathcal{V}_0$ . (symmetry constraints)

• the formation potential

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the symmetry potential

$$F_s(p(t)) = \frac{1}{2} \sum_{i \in \mathcal{V}_0} \sum_{\substack{u,v \in \Gamma_i \\ uv \in \mathcal{E}}} \|p_u(t) - \tau(\gamma_{vu})p_v(t)\|^2$$

# **Assumption 1**

The sub-graph induced by each vertex orbit  $\Gamma_i$  is connected.

the formation potential

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· the symmetry potential

$$F_s(p(t)) = \frac{1}{2} \sum_{i \in \mathcal{V}_0} \sum_{\substack{u,v \in \Gamma_i \\ uv \in \mathcal{E}}} ||p_u(t) - \tau(\gamma_{vu})p_v(t)||^2$$

# **Assumption 1**

The sub-graph induced by each vertex orbit  $\Gamma_i$  is connected.

the symmetric formation potential

$$F(p(t)) = F_f(p(t)) + F_s(p(t))$$

· propose the gradient control

$$u(t) = -\nabla F(p(t))$$

propose the gradient control

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closed-loop dynamics

$$\dot{p}(t) = -R(p(t))^T \left( R(p(t))p(t) - \mathbf{d}^2 \right) - Qp(t)$$

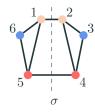
where Q is symmetric and a block-diagonal matrix with

$$[Q_i]_{uv} = \begin{cases} d_{\Gamma_i}(u)I, & u = v, \ u \in \Gamma_i \\ -\tau(\gamma_{uv}), & uv \in \mathcal{E}, u, v \in \Gamma_i \\ 0, & \text{o.w.} \end{cases} \quad \begin{array}{ll} \bullet & Q_i \in \mathbb{R}^{|\Gamma_i|d \times |\Gamma_i|d} \\ \bullet & [Q]_{uv} \in O(\mathbb{R}^d) \text{ (orthogonal group)} \\ \bullet & \tau(\gamma_{uv})^{-1} = \tau(\gamma_{uv})^T \end{cases}$$

- $\circ \ Q_i$  has a decomposition  $Q_i = E(\Gamma_i)E(\Gamma_i)^T$
- $\circ \ Q = \bar{E}(\Gamma)\bar{E}(\Gamma)^T$
- $\circ$  any p in a symmetric position satisfies Qp=0

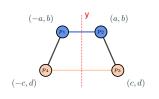
# "NICE" GRAPHS

- symmetric formation potential makes no assumption on relation between the graph  $\mathcal G$  and the point group  $\tau(\Gamma)$
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• 
$$\Gamma = \{ \mathrm{Id}, \psi_4 \} \subseteq \mathrm{Aut}(\mathcal{G})$$

• 
$$\Gamma_1 = \Gamma_2 = \{1, 2\}, \ \Gamma_3 = \Gamma_4 = \{3, 4\}$$

• 
$$V_0 = \{1, 4\}$$

• isometry 
$$\tau(\gamma):(a,b)\mapsto (-a,b)$$

satisfies  $au(\gamma)(p_i)=p_{\gamma(i)}$  for all  $i\in\mathcal{V}$  and for each  $i\in\mathcal{V}_0$  and  $j\in\Gamma_i\setminus\{i\}$ , the edge ij is in  $\mathcal{E}$  (i.e.  $\mathcal{G}(\Gamma_i)$  is connected)

· propose the gradient control

$$u(t) = -\nabla F(p(t))$$

closed-loop dynamics

$$\dot{p}(t) = -R(p(t))^T \left( R(p(t))p(t) - \mathbf{d}^2 \right) - Qp(t)$$

· dynamics for each agent

$$\left[\dot{p}_i(t) = \sum_{ij \in \mathcal{E}} (\|p_i(t) - p_j(t)\|^2 - \mathbf{d}_{ij}^2) (p_j(t) - p_i(t)) + \sum_{\substack{ij \in \mathcal{E} \\ i,j \in \Gamma_u}} (\tau(\gamma_{ij}) p_j(t) - p_i(t))\right]$$

# Theorem [Z, Shulze, Tanigawa '23]

Consider a team of n integrator agents interacting over a  $\Gamma$ -symmetric graph  $\mathcal G$  satisfying Assumption 1 that can be drawn with maximum point group symmetry  $\mathcal S$  in  $\mathbb R^d$ , and let

$$\mathcal{F}_f = \{ p \in \mathbb{R}^{dn} \mid ||p_i - p_j|| = \mathbf{d}_{ij} \ ij \in \mathcal{E} \}, \ \text{and} \ \mathcal{F}_s = \{ p \in \mathbb{R}^{dn} \mid \tau(\gamma)(p_i) = p_{\gamma(i)} \ \forall \gamma \in \Gamma, \ i \in \mathcal{V} \}.$$

Then for initial conditions  $p_i(0)$  satisfying

$$\sum_{ij\in\mathcal{E}} (\|p_i(0) - p_j(0)\| - \mathbf{d}_{ij})^2 \le \epsilon_1, \text{ and } \|p_i(0) - \tau(\gamma_{ij})p_j(0)\|^2 \le \epsilon_2$$

for all  $i,j\in\Gamma_u$  and  $u\in\mathcal{V}_0$ , for a sufficiently small and positive constant  $\epsilon_1$  and  $\epsilon_2$ , the control

$$u = -\nabla F(p(t)),$$

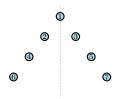
renders the set  $\mathcal{F}_f \cap \mathcal{F}_s$  exponentially stable, i.e.

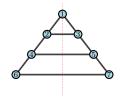
$$\lim_{t\to\infty} \|p_i(t)-p_j(t)\| = \mathbf{d}_{ij} \text{ and } \lim_{t\to\infty} \tau(\gamma)(p_i(t)) = \lim_{t\to\infty} p_{\gamma(i)}(t) \quad \text{for all } \gamma\in\Gamma, i\in\mathcal{V}.$$

### **EXAMPLE: THE VIC FORMATION**

- formation flight for aircraft originated in WWI
- Vic formation used by pilots to improve visual communication and defensive advantages



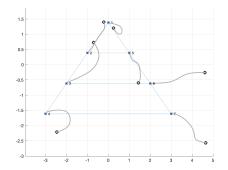




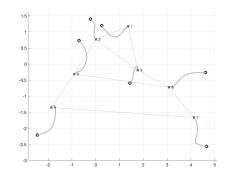
Vic formation with symmetry Flexible framework (9 edges; mirror satisfies Assumption 1)

Minimally Rigid framework (11 edges)

#### **EXAMPLE: THE VIC FORMATION**



- symmetry constraints force agents to correct formation
- requires less agent communication than standard formation control with MIR requirement



 with flexible framework and only formation potential can not guarantee convergence to correct shape

### **EXPLOIT MORE SYMMETRY**

 $\bullet\,$  proposed strategy does not take advantage of the full power of symmetry

### **EXPLOIT MORE SYMMETRY**

- proposed strategy does not take advantage of the full power of symmetry
- can we find redundant information between the symmetry constraints and the distance constraints?

### $\Gamma$ -SYMMETRIC FRAMEWORK

### **Definition**

An infinitesimal motion u of a  $\tau(\Gamma)$ -symmetric framework  $(\mathcal{G},p)$  is  $\tau(\Gamma)$ -symmetric if

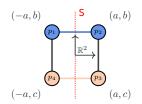
$$\tau(\gamma)(u_i) = u_{\gamma(i)}$$
 for all  $\gamma \in \Gamma$  and all  $i \in \mathcal{V}$ . (1)

We say that  $(\mathcal{G}, p)$  is  $\tau(\Gamma)$ -symmetric infinitesimally rigid if every  $\tau(\Gamma)$ -symmetric infinitesimal motion is trivial.

infinitesimal motions can also be studied in this framework

- $\tau(\gamma)(u_i) = u_{\gamma(i)}$
- understanding symmetry structure means we only need to find infintesimal motion for one representative vertex in each vertex orbit

### **ORBIT RIGIDITY MATRIX**



$$R(p) = \begin{bmatrix} (-2a & 0) & (2a & 0) & (0 & 0) & (0 & 0) \\ (0 & b - c) & (0 & 0) & (0 & 0) & (0 & c - b) \\ (0 & 0) & (0 & b - c) & (0 & c - b) & (0 & 0) \\ (0 & 0) & (0 & 0) & (-2a & 0) & (2a & 0) \end{bmatrix}$$

Due to symmetry, certain rows and columns of the rigidity matrix are redundant.

# Orbit Rigidity Matrix $\mathcal{O}(\mathcal{G}_0,p)$

[Schulze 2011]

$$\mathcal{O}(\mathcal{G}_0, p) = \begin{bmatrix} (2p_1 - \tau_s p_1 - \tau_s^{-1} p_1)^T & (0 & 0) \\ (p_1 - p_4)^T & (p_4 - p_1)^T \\ (0 & 0) & (2p_4 - \tau_s p_4 - \tau_s^{-1} p_4)^T \end{bmatrix} = \begin{bmatrix} (-2a & 0) & (0 & 0) \\ (b - c) & (c - b) \\ (0 & 0) & (-2a & 0) \end{bmatrix}$$

Describes the  $\tau(\Gamma)$ -symmetric infinitesimal rigidity properties of  $\tau(\Gamma)$ -symmetric frameworks.

The introduction of the orbit rigidity matrix suggests a further way to exploit symmetries in formation control:

- · Only representative edges are required to maintain distances
- Symmetries within vertex orbits have no need for distance constraints

### **QUOTIENT GAIN GRAPHS**

- relation between vertices within vertex orbits and between vertex orbits (through edge orbits) captured by quotient gain graph of a  $\Gamma$ -symmetric graph
  - node set is representative vertex set  $\mathcal{V}_0$
  - edge set is representative edge set  $\mathcal{E}_0$ : choose edge of form  $i\gamma(j)$  with  $i,j\in\mathcal{V}_0$

```
it is ok for i = j
```

edges are directed with 'edge gain' being the group action  $\gamma \in \Gamma$ 

# **QUOTIENT GAIN GRAPHS**

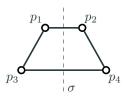


• 
$$\Gamma = \{ \mathrm{Id}, \psi_1 \}$$
 (rotation)

• 
$$\Gamma_i = \{1, 2, 3, 4\}$$

• 
$$V_0 = \{1\}$$
,  $\mathcal{E}_0 = \{e_1\}$ 





- $\Gamma = \{ \mathrm{Id}, \psi_4 \}$  (reflection)
- $\Gamma_{1,2} = \{1,2\}$ ,  $\Gamma_{3,4} = \{3,4\}$
- $\mathcal{V}_0 = \{1, 3\}$ ,  $\mathcal{E}_0 = \{12, 13, 24\}$





- $\Gamma = \{ \mathrm{Id}, \psi_6 \}$  (reflection)
- $\Gamma_1 = \{1\}$ ,  $\Gamma_4 = \{4\}$ ,  $\Gamma_{2,3} = \{2,3\}$
- $V_0 = \{1, 3, 4\}, \mathcal{E}_0 = \{13, 14\}$



Definition [Shulze 2011]

The orbit rigidity matrix  $\mathcal{O}(\mathcal{G}_0, \bar{p})$  of  $(\mathcal{G}, p)$  is the  $|\mathcal{E}_0| \times d|\mathcal{V}_0|$  matrix defined as follows. The row corresponding to an edge  $((i, j); \gamma)$ , where  $i \neq j$ , has the form:

$$\left( \begin{array}{ccc} 0 \cdots 0 & (\bar{p}_i - \tau(\gamma)\bar{p}_j)^T & 0 \cdots 0 & (\bar{p}_j - \tau(\gamma)^{-1}\bar{p}_i)^T & 0 \cdots 0 \end{array} \right),$$

with the d-dimensional entries  $(\bar{p}_i - \tau(\gamma)\bar{p}_j)^T$  and  $(\bar{p}_j - \tau(\gamma)^{-1}\bar{p}_i)^T$  being in the columns corresponding to vertex i and j, respectively. The row corresponding to a loop  $((i,i);\gamma)$  has the form:

$$\left(\begin{array}{cc} 0\cdots 0 & (2\bar{p}_i - \tau(\gamma)\bar{p}_i - \tau(\gamma)^{-1}\bar{p}_i)^T & 0\cdots 0 \end{array}\right),$$

with the d-dimensional entry  $(2\bar{p}_i - \tau(\gamma)\bar{p}_i - \tau(\gamma)^{-1}\bar{p}_i)^T$  being in the columns corresponding to vertex i.

Theorem [Shulze 2011]

Let  $(\mathcal{G},p)$  be a  $\tau(\Gamma)$ -symmetric framework with orbit rigidity matrix  $\mathcal{O}(\mathcal{G}_0,\bar{p})$ . Then,

- (i) the kernel of  $\mathcal{O}(\mathcal{G}_0, \bar{p})$  is isomorphic to the space of  $\tau(\Gamma)$ -symmetric infinitesimal motions of  $(\mathcal{G}, p)$ , and
- (ii) the cokernel of  $\mathcal{O}(\mathcal{G}_0, \bar{p})$  is isomorphic to the space of  $\tau(\Gamma)$ -symmetric self-stresses of  $(\mathcal{G}, p)$ .
  - · Orbit rigidity matrix can be used to identify symmetric infinitesimal flexes
  - full-rank  $\mathcal{O}(\mathcal{G}_0, \bar{p})$  implies none exist
  - size of  $\mathcal{O}(\mathcal{G}_0,\bar{p})$  does not depend on p, but only the graph and symmetry constraints
  - $\tau(\Gamma)$ -isostatic frameworks have orbit rigidity matrices with full row-rank

### **ORBIT RIGIDITY MATRIX**

key point: quotient gain graph and orbit rigidity matrix suggests a further way to exploit symmetry in formation control

- · representative edges used to maintain distances
- · symmetry within vertex orbits have no need for distance constraints

### A MODIFIED FORMATION POTENTIAL

· the representative edge formation potential

$$F_e(p(t)) = \frac{1}{4} \sum_{e=ij \in \mathcal{E}_0} (\|p_i - \tau(\gamma)p_j\|^2 - \mathbf{d}_{i\gamma(j)}^2)^2$$

 $\circ \ \gamma$  is label of edge in quotient gain graph

#### A MODIFIED FORMATION POTENTIAL

the representative edge formation potential

$$F_e(p(t)) = \frac{1}{4} \sum_{e=ij \in \mathcal{E}_0} \left( \|p_i - \tau(\gamma)p_j\|^2 - \mathbf{d}_{i\gamma(j)}^2 \right)^2$$

- $\circ \ \gamma$  is label of edge in quotient gain graph
- · the symmetry potential

$$F_s(p(t)) = \frac{1}{2} \sum_{i \in \mathcal{V}_0} \sum_{\substack{u,v \in \Gamma_i \\ uv \in \mathcal{E}}} \|p_u(t) - \tau(\gamma_{vu})p_v(t)\|^2$$

# **Assumption 1**

The sub-graph induced by each vertex orbit  $\Gamma_i$  is connected.

### A MODIFIED FORMATION POTENTIAL

the representative edge formation potential

$$F_e(p(t)) = \frac{1}{4} \sum_{e=ij \in \mathcal{E}_0} \left( \|p_i - \tau(\gamma)p_j\|^2 - \mathbf{d}_{i\gamma(j)}^2 \right)^2$$

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# **Assumption 1**

The sub-graph induced by each vertex orbit  $\Gamma_i$  is connected.

the symmetric formation potential

$$F(p(t)) = F_e(p(t)) + F_s(p(t))$$

### A MODIFIED FORMATION CONTROL

• node relabeling - representative vertices first

$$\tilde{p} = Pp = \begin{bmatrix} p_o^T & p_f^T \end{bmatrix}^T$$

· propose the gradient control

$$u(t) = -\nabla F(p(t))$$

Then the control for each agent  $i \in \mathcal{V}_0$  can be expressed as

$$u_i(t) = u_i^{(a)}(t) + u_i^{(b)}(t) + u_i^{(c)}(t),$$
 (2)

where

$$\begin{split} u_i^{(a)}(t) &= \sum_{\substack{i\gamma(j) \in \mathcal{E}_0 \\ j \in \mathcal{V}_0, \ i \neq j}} \left( \|p_i(t) - \tau(\gamma)p_j(t)\|^2 - \mathbf{d}_{ij}^2 \right) (\tau(\gamma)p_j(t) - p_i(t)) \\ u_i^{(b)}(t) &= -\sum_{\substack{i\gamma(i) \in \mathcal{E}_0 \\ i \neq i}} (\|(I - \tau(\gamma))p_i\|^2 - \mathbf{d}_{i\gamma(i)}^2) (2I - \tau(\gamma) - \tau(\gamma)^{-1}) p_i \\ u_i^{(c)}(t) &= \sum_{\substack{ij \in \mathcal{E}(\Gamma_i)}} (\tau(\gamma_{ij})p_j(t) - p_i(t)). \end{split}$$

The control for the agents in  $V \setminus V_0$  is simply

$$u_i(t) = \sum_{ij \in \mathcal{E}(\Gamma_u)} (\tau(\gamma_{ij}) p_j(t) - p_i(t)), \tag{3}$$

for each  $u \in \mathcal{V}_0$ .

in state-space form

$$\begin{bmatrix} \dot{p}_0(t) \\ \dot{p}_f(t) \end{bmatrix} = \begin{bmatrix} -\mathcal{O}^T(\mathcal{G}_0, p_0(t)) \begin{pmatrix} \mathcal{O}(\mathcal{G}_0, p_0(t)) p_0(t) - \mathbf{d}_0^2 \\ 0 \end{pmatrix} \end{bmatrix} - PQP^T \begin{bmatrix} p_0(t) \\ p_f(t) \end{bmatrix}$$

recall our earlier idea

$$\dot{p}(t) = -R(p(t))^T \left( R(p(t))p(t) - \mathbf{d}^2 \right) - Qp(t)$$

we can define an error system with

$$e = \begin{bmatrix} \sigma \\ q \end{bmatrix} = \begin{bmatrix} \mathcal{O}(\mathcal{G}_0, p_0(t)) p_0(t) - \mathbf{d}_0^2 \\ \bar{E}(\Gamma)^T P^T p(t) \end{bmatrix}$$

orbit error dynamics

$$\begin{bmatrix} \dot{\bar{\sigma}}(t) \\ \dot{\bar{q}}(t) \end{bmatrix} = - \begin{bmatrix} \mathcal{O}\mathcal{O}^T & \mathcal{O}\bar{E}_0(\Gamma) \\ \bar{E}_0^T(\Gamma)\mathcal{O}^T & \bar{E}^T(\Gamma)\bar{E}(\Gamma) \end{bmatrix} \begin{bmatrix} \bar{\sigma}(t) \\ \bar{q}(t) \end{bmatrix}$$

$$= - \begin{bmatrix} \begin{bmatrix} \mathcal{O} & 0 \\ \bar{E}^T(\Gamma)P^T \end{bmatrix} \begin{bmatrix} \begin{bmatrix} \mathcal{O}^T \\ 0^T \end{bmatrix} P\bar{E}(\Gamma) \end{bmatrix} \begin{bmatrix} \bar{\sigma}(t) \\ \bar{q}(t) \end{bmatrix}.$$

#### **MAIN RESULT**

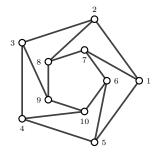
### **Theorem**

Let  ${\bf p}$  be the target formation satisfying conditions (i) and (ii) of the Symmetry-Forced Formation Control Problem, and assume that  $({\cal G},{\bf p})$  is a  $\tau(\Gamma)$ -symmetric isostatic framework. Then the origin is a locally exponentially stable equilibrium of the orbit error dynamics.

### **Theorem**

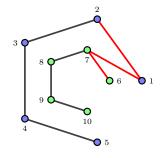
The orbit rigidity control uses at most  $(1+1/|\Gamma|)|\mathcal{V}|$  edges.

• can be significantly less than  $2|\mathcal{V}|-3$ 





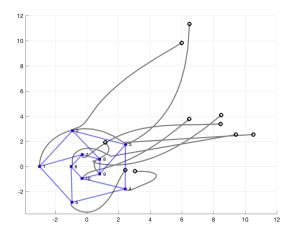
- at least 17 edges required for infinitesimal rigidity
- · flexible framework





quotient gain graph

- $2\pi/5$  rotational symmetry
- can use only spanning tree subgraph for each vertex orbit
- only 3 distances required



• nice...but symmetries are defined with respect to a global origin

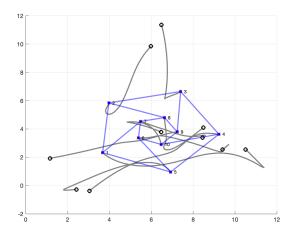
idea: augment a virtual consensus dynamics

$$\begin{bmatrix} \dot{p}_0(t) \\ \dot{p}_f(t) \end{bmatrix} = \begin{bmatrix} -\mathcal{O}^T(\mathcal{G}_0, c_0(t)) \left( \mathcal{O}(\mathcal{G}_0, c_0(t)) c_0(t) - \mathbf{d}_0^2 \right) \\ 0 \end{bmatrix} - PQP^T \begin{bmatrix} c_0(t) \\ c_f(t) \end{bmatrix}$$
$$\dot{r} = -L(\mathcal{G})r$$

with 
$$c(t) = p(t) - r(t)$$

- · cascade structure
- same analysis idea

# **CENTROID CONSENSUS**



### **FORMATION MANEUVERING**

• translational maneuvering: virtual state with PI consensus filter

$$\begin{cases} \dot{\bar{r}} &= -k_P \bar{L}(\mathcal{G})\bar{r} - k_I \bar{L}(\mathcal{G})\bar{\zeta} + nB \otimes v_0(t) \\ \dot{\bar{\zeta}} &= \bar{L}(\mathcal{G})\bar{r} \end{cases}$$



### **FORMATION MANEUVERING**

• rotational maneuvering: tranformation of  $\tau(\gamma)$  by known rotation matrix

$$\left(\tau(\gamma, \theta(t)) = R(\theta(t))\tau(\gamma)R(\theta(t))^{-1}\right)$$



### **CONCLUDING REMARKS**

# **Summary**

- $au(\Gamma)$ -symmetric graphs captures symmetry of configurations and graphs
- symmetric formation potential used to design distributed control law with less edges compared to "traditional" formation control strategies
- opportunities for more sophisticated motion coordination

Zelazo, Tanigawa and Shulze, Forced Symmetric Formation Control, IEEE Transactions on Control of Network Systems (early access).

### **Future Work**

- formation maneuvering requires time-varying point group symmetries
- is it possible to distributedly decide on certain symmetries?
- · can we eliminate need for requiring self-state in protocol?
- · more?

# **Questions?**

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