

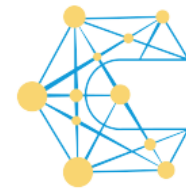
SYMMETRY-CONSTRAINED FORMATION MANEUVERING

64th ISRAEL ANNUAL CONFERENCE ON AEROSPACE SCIENCES

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Department of Aerospace Engineering

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CONNECT LAB
Cooperative Networks and Controls

FORMATION CONTROL - INTRODUCTION

Many applications require multiple agents to organize into specific spatial formations.

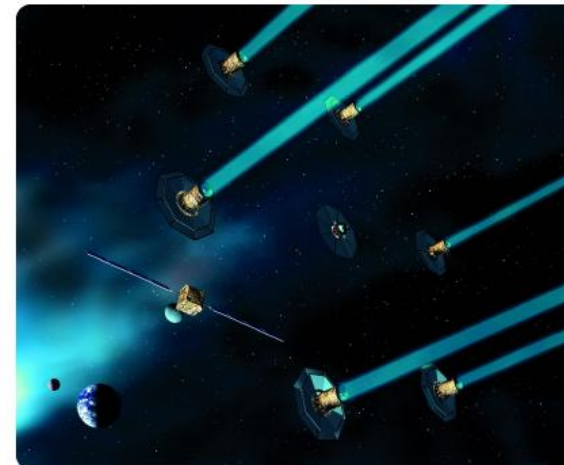
- UAV Formations

- Surveillance
- Aerial Transportation
- Communication Networks



- Spacecraft formations

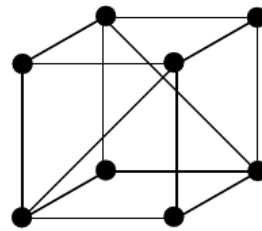
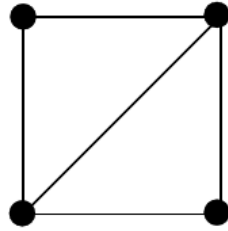
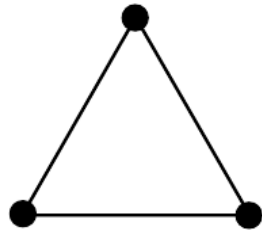
- Interferometry
- Constellations for sensing



FORMATION CONTROL - OBJECTIVE

Given a team of agents able to sense/communicate with neighboring agents:

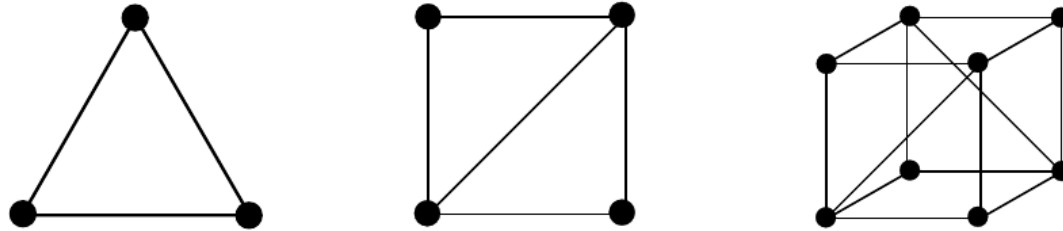
- Design a control strategy for each agent by using *only* local information to achieve a desired spatial configuration - **Formation Aquisition**



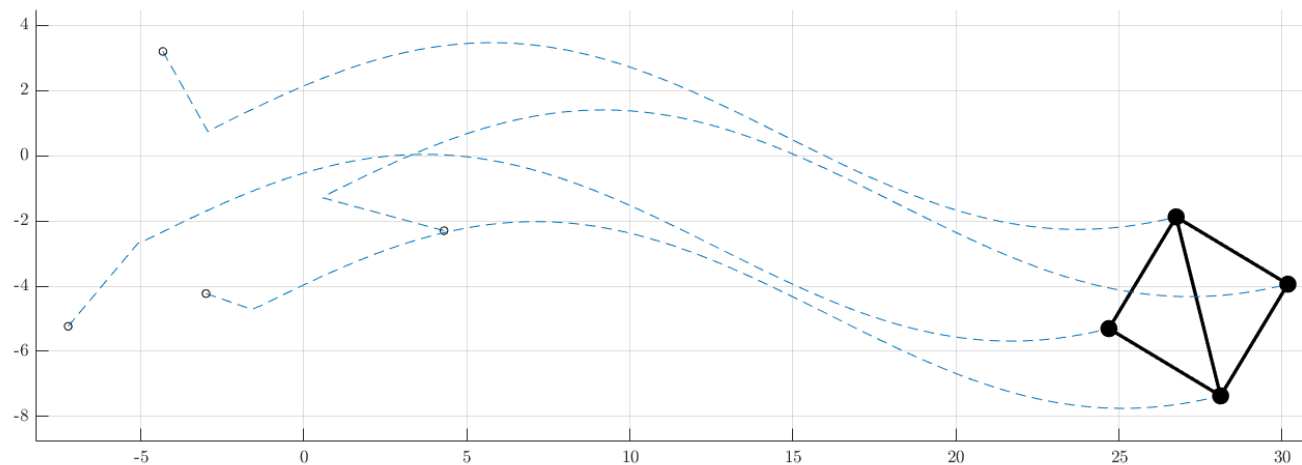
FORMATION CONTROL - OBJECTIVE

Given a team of agents able to sense/communicate with neighboring agents:

- Design a control strategy for each agent by using *only* local information to achieve a desired spatial configuration - **Formation Acquisition**



- Simultaneously move the formation through space as a rigid body - **Formation Maneuvering**

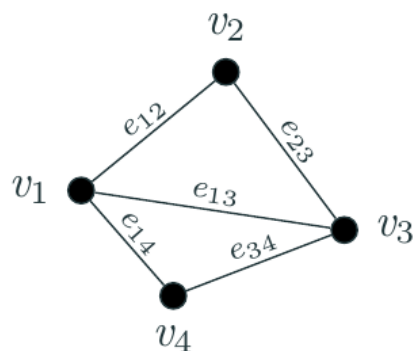


FORMATION CONTROL - AGENT CONFIGURATION

Consider a team of n agents, where the position of the i th agent is given by $p_i(t) \in \mathbb{R}^d$. Each follows the simple integrator dynamics:

$$\dot{p}_i(t) = u_i(t)$$

- The agents interact according to an information exchange graph $\mathcal{G} = (\mathcal{V}, \mathcal{E})$

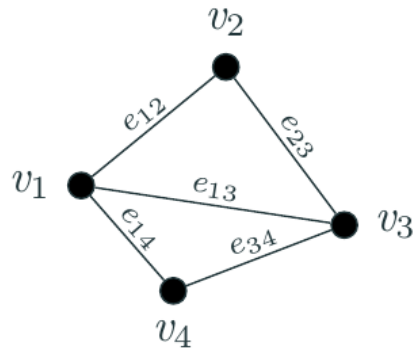


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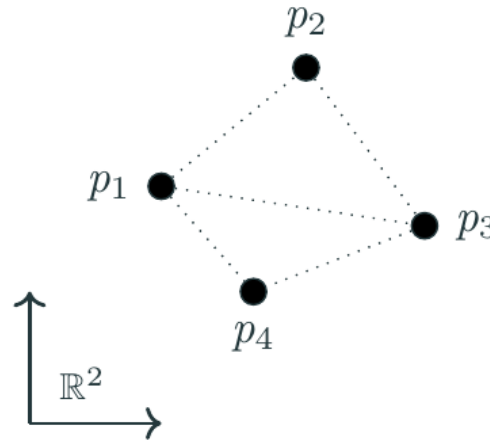
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- The **framework** - (\mathcal{G}, p) embeds the graph in Euclidean space

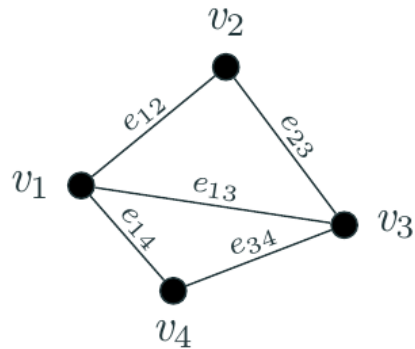


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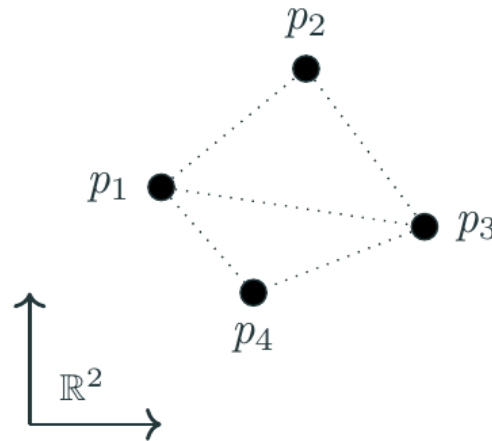
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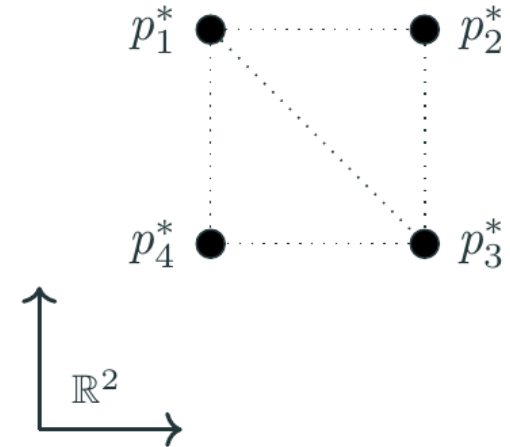
- The agents interact according to an information exchange graph $\mathcal{G} = (\mathcal{V}, \mathcal{E})$



- The **framework** - (\mathcal{G}, p) embeds the graph in Euclidean space



- The desired formation is represented by the framework (\mathcal{G}, p^*)



FORMATION CONTROL - CONSTRAINTS

- The **desired formation** is characterized by a set of M constraints, encoded in the function $F : \mathbb{R}^{nd} \rightarrow \mathbb{R}^M$, and a configuration \mathbf{p}^* satisfying the constraints.
- The set of all **feasible formations** is

$$\mathcal{F}(p) = \{p \in \mathbb{R}^{nd} \mid F(p) = F(\mathbf{p}^*)\}$$

Formation Control Objective

For an ensemble of n agents with dynamics

$$\dot{p}_i = u_i,$$

with $p_i(t) \in \mathbb{R}^d$, an information exchange graph $\mathcal{G} = (\mathcal{V}, \mathcal{E})$, and formation constraint function $F : \mathbb{R}^{nd} \rightarrow \mathbb{R}^M$, design a distributed control law for each agent $i \in \{1, \dots, n\}$ such that the set

$$\mathcal{F}(p) = \{p \in \mathbb{R}^{nd} \mid F(p) = F(\mathbf{p}^*)\},$$

is asymptotically stable.

Theorem - Distance Constrained Formation Control

[Krick 2009]

Consider the potential function

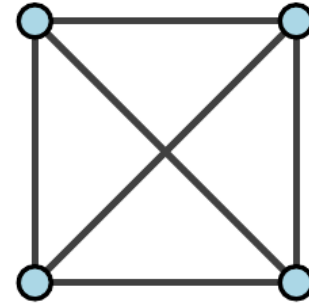
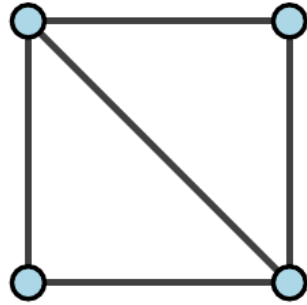
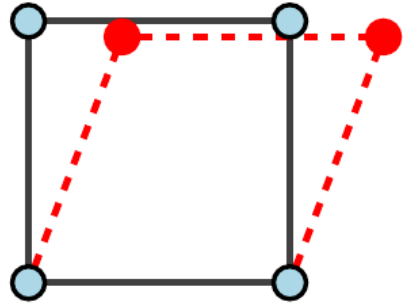
$$F_f(p) = \frac{1}{4} \sum_{ij \in \mathcal{E}} (\|p_i(t) - p_j(t)\|^2 - (d_{ij}^*)^2)^2$$

and assume the desired distances d_{ij}^* correspond to a feasible formation. Then the gradient dynamical system

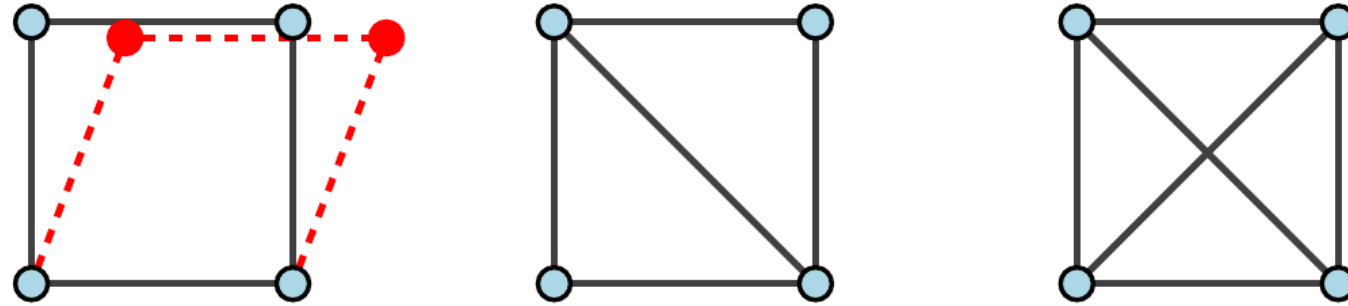
$$\dot{p}_i = u_i = -\nabla_{p_i} F_f(p) = \sum_{ij \in \mathcal{E}} (\|p_i - p_j\|^2 - (d_{ij}^*)^2) (p_j - p_i)$$

asymptotically converges to the critical points of the potential function, i.e., $\frac{\partial F_f(p)}{\partial p} = 0$.

How do we define shapes ?

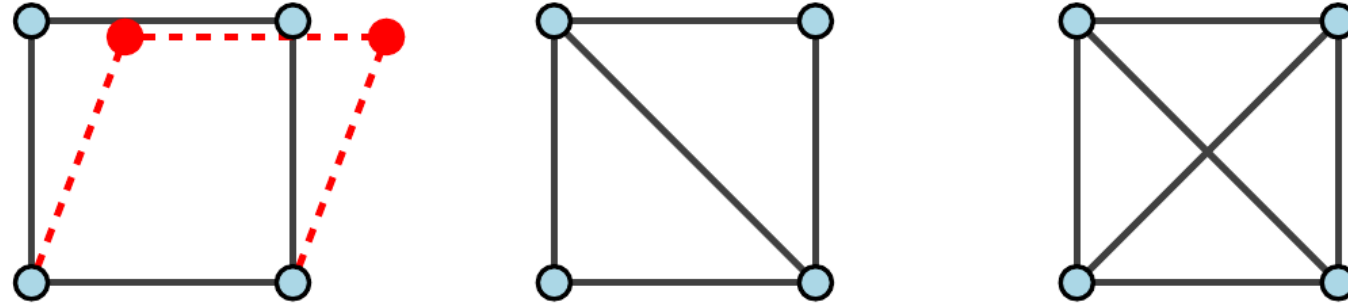


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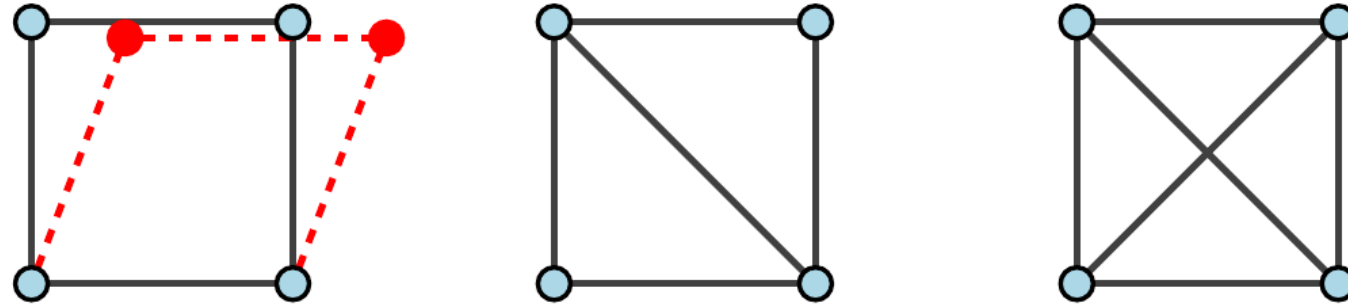
- **Rigidity Theory** allows us to determine:
 - the number of constraints required to ensure the desired shape.
 - how the constraints should be distributed on the network.

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- **Rigidity Theory** allows us to determine:
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 - how the constraints should be distributed on the network
- $R(p) = \frac{\partial F(p)}{\partial p} = \text{diag}(p_i - p_j)(E^T \otimes I_d)$, the **rigidity matrix** of (\mathcal{G}, p) , where E is the incidence matrix of \mathcal{G}
 - A framework is **infinitesimally rigid** if and only if $\text{rk} R(p) = 2n - 3$ in \mathbb{R}^2
 - property that ensures formations defined properly

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 - A framework is **infinitesimally rigid** if and only if $\text{rk}R(p) = 2n - 3$ in \mathbb{R}^2
 - property that ensures formations defined properly

$$\dot{p} = -\nabla_p F_f(p) = -R^T(p) (R(p)p - (d^*)^2)$$

- Properties of the rigidity matrix lead to an architectural requirement for formation control problems, ensuring that the controller converges to the correct formation shape. Equivalent to:

$$\text{rk } R(p) = 2|\mathcal{V}| - 3 \text{ and } |\mathcal{E}| = 2|\mathcal{V}| - 3 \quad (\text{in } \mathbb{R}^2)$$

Q: Can the problem be solved with fewer constraints ?

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Q: Can the problem be solved with fewer constraints ?

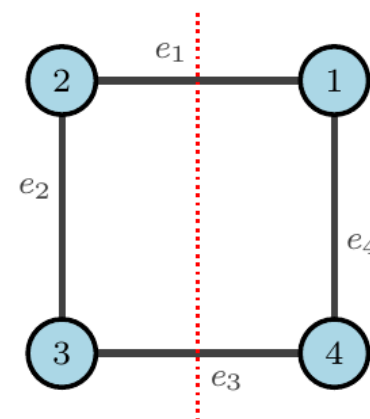
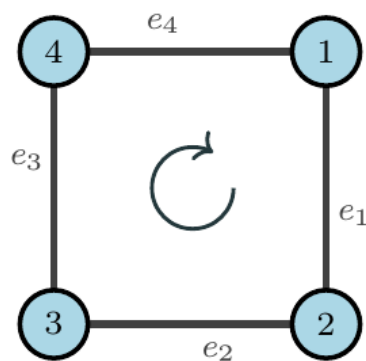
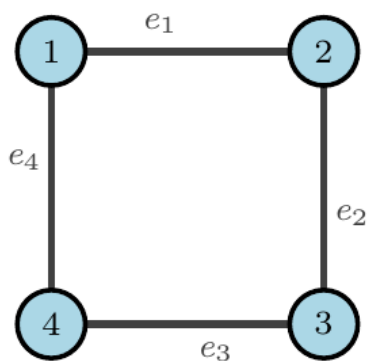
A: Yes, by additionally implementing symmetry constraints!

SYMMETRY AND GRAPH AUTOMORPHISMS

Graph Automorphism

An **automorphism** of the graph $\mathcal{G} = (\mathcal{V}, \mathcal{E})$ is a permutation $\psi : \mathcal{V} \rightarrow \mathcal{V}$ of its vertex set such that

$$\{v_i, v_j\} \in \mathcal{E} \Leftrightarrow \{\psi(v_i), \psi(v_j)\} \in \mathcal{E}$$



Identity:

$$\text{Id} = \begin{pmatrix} 1 & 2 & 3 & 4 \\ 1 & 2 & 3 & 4 \end{pmatrix}$$

90° rotation:

$$\psi_1 = \begin{pmatrix} 1 & 2 & 3 & 4 \\ 2 & 3 & 4 & 1 \end{pmatrix}$$

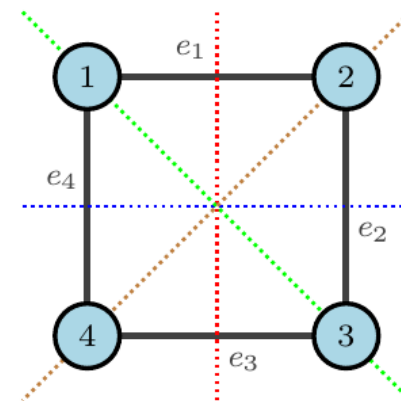
reflection:

$$\psi_2 = \begin{pmatrix} 1 & 2 & 3 & 4 \\ 2 & 1 & 4 & 3 \end{pmatrix}$$

Automorphisms encode graph **symmetries**

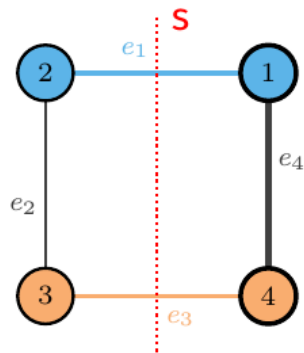
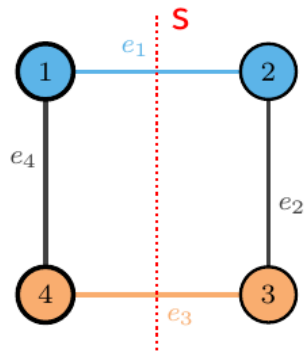
AUTOMORPHISM GROUPS

- Additional permutations can be found for the given graph considering all possible reflections and rotations (by 180° and 270°)
- The set of all automorphisms of \mathcal{G} form a *group* - $\text{Aut}(\mathcal{G})$
 - $\text{Aut}(\mathcal{G}) = \{\text{Id}, \psi_1, \psi_2, \dots\}$
- A **subgroup** is a subset of a group, satisfying all properties of a group
 - $\{\text{Id}, \psi_1\}$
 - $\{\text{Id}, \psi_2\}$
- Subgroups of $\text{Aut}(\mathcal{G})$ define specific symmetries in \mathcal{G}
- for any subgroup $\Gamma \subseteq \text{Aut}(\mathcal{G})$, we say that \mathcal{G} is **Γ -symmetric**



Definition

For a Γ -symmetric graph $\mathcal{G} = (\mathcal{V}, \mathcal{E})$ and vertex $i \in \mathcal{V}$, the set $\Gamma_i = \{\gamma(i) \mid \gamma \in \Gamma\}$ is called the **vertex orbit** of i . Similarly, for an edge $e = ij \in \mathcal{E}$, the set $\Gamma_e = \{\gamma(i)\gamma(j) \mid \gamma \in \Gamma\}$ is termed the **edge orbit** of e .



consider $\Gamma = \{\text{Id}, \psi_2\}$ (reflection about mirror s)

- **Vertex Orbit:**

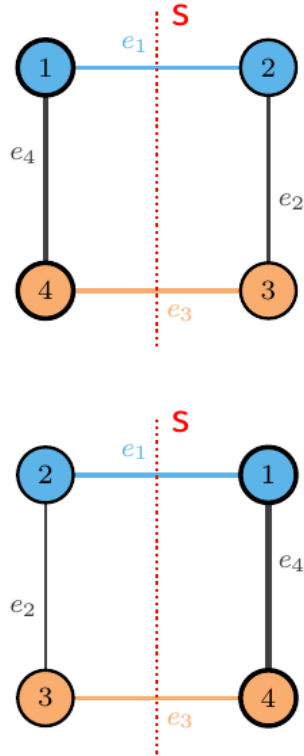
$$\Gamma_1 = \Gamma_2 = \{1, 2\}, \quad \Gamma_3 = \Gamma_4 = \{3, 4\}$$

- **Edge Orbit:**

$$\Gamma_{e_1} = \{e_1\}, \quad \Gamma_{e_3} = \{e_3\}, \quad \Gamma_{e_2} = \Gamma_{e_4} = \{e_2, e_4\}$$

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- **Vertex Orbit:**

$$\Gamma_1 = \Gamma_2 = \{1, 2\}, \Gamma_3 = \Gamma_4 = \{3, 4\}$$

vertices inside a vertex orbit are equivalent

representative vertex set: $\mathcal{V}_0 = \{1, 4\}$

- **Edge Orbit:**

$$\Gamma_{e_1} = \{e_1\}, \Gamma_{e_3} = \{e_3\}, \Gamma_{e_2} = \Gamma_{e_4} = \{e_2, e_4\}$$

edges inside an edge orbit are equivalent

representative edge set: $\mathcal{E}_0 = \{e_1, e_3, e_4\}$

$\tau(\Gamma)$ -SYMMETRIC FRAMEWORKS

Let Γ be represented as a point group.

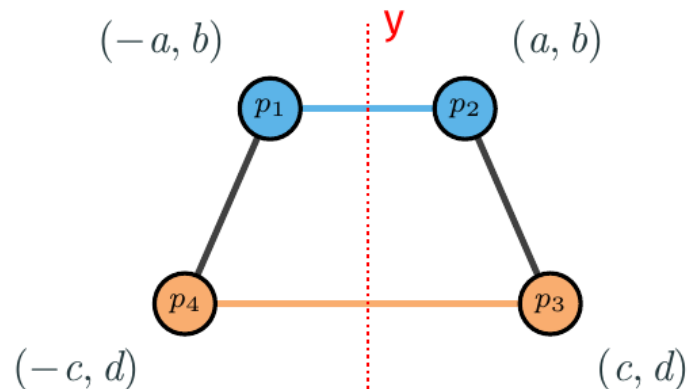
- homomorphism $\tau : \Gamma \rightarrow O(\mathbb{R}^d)$
- τ assigns an orthogonal matrix (describing an isometry of \mathbb{R}^d) to each element of Γ

Definition

A framework (\mathcal{G}, p) in \mathbb{R}^d is called $\tau(\Gamma)$ -symmetric if

$$\tau(\gamma)(p_i) = p_{\gamma(i)} \quad \text{for all } \gamma \in \Gamma \text{ and all } i \in \mathcal{V}.$$

For example

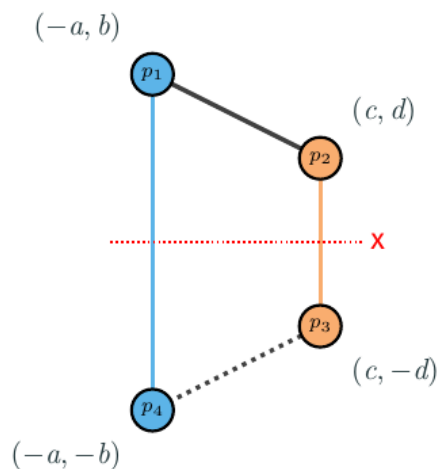


- consider $\Gamma = \{\text{Id}, \psi_2\} \subseteq \text{Aut}(\mathcal{G})$

- isometry $\tau(\psi_2) = \begin{bmatrix} -1 & 0 \\ 0 & 1 \end{bmatrix} : \tau(\psi_2) \begin{bmatrix} -a \\ b \end{bmatrix} = \begin{bmatrix} a \\ b \end{bmatrix}$

isometries of the desired configuration coincide with symmetries of the automorphisms of \mathcal{G}

ORBIT RIGIDITY MATRIX



The rigidity matrix:

$$R(p) = \begin{bmatrix} (-a - c & b - d) & (c + a & d - b) & (0 & 0) & (0 & 0) \\ (0 & 2b) & (0 & 0) & (0 & 0) & (0 & -2b) \\ (0 & 0) & (0 & 2d) & (0 & -2d) & (0 & 0) \\ (0 & 0) & (0 & 0) & (c + a & -d + b) & (-a - c & -b + d) \end{bmatrix}$$

Symmetries make certain rows and columns of the rigidity matrix redundant

Orbit Rigidity Matrix $\mathcal{O}(\mathcal{G}_0, p)$

[Schulze 2011]

$$\mathcal{O}(\mathcal{G}_0, p) = \begin{bmatrix} (p_1 - p_2)^T & (p_2 - p_1)^T \\ (2p_1 - \tau_x p_1 - \tau_x^{-1} p_1)^T & (0 \ 0) \\ (0 \ 0) & (2p_2 - \tau_x p_2 - \tau_x^{-1} p_2)^T \end{bmatrix} = \begin{bmatrix} (-a - c & b - d) & (c + a & d - b) \\ (0 & 2b) & (0 & 0) \\ (0 & 0) & (0 & 2d) \end{bmatrix}$$

Describes the $\tau(\Gamma)$ -symmetric infinitesimal rigidity properties of $\tau(\Gamma)$ -symmetric frameworks.

The introduction of the **orbit rigidity matrix** suggests a further way to exploit symmetry in formation control

- representative edges used to maintain distances
- symmetry within vertex orbits have no need for distance constraints

A GRADIENT APPROACH

Similar to traditional rigidity approaches, define a *symmetric formation potential*

$$F_f(p(t)) = F_e(p(t)) + F_s(p(t))$$

where

- The representative edge formation potential:

$$F_e(p(t)) = \frac{1}{4} \sum_{ij \in \mathcal{E}_0} \left(\|p_i(t) - \tau(\gamma)p_j(t)\|^2 - (d_{i\gamma(j)}^*)^2 \right)^2$$

- The symmetry potential:

$$F_s(p(t)) = \frac{1}{2} \sum_{i \in \mathcal{V}_0} \sum_{\substack{u, v \in \Gamma_i \\ uv \in \mathcal{E}}} \|p_u(t) - \tau(\gamma_{vu})p_v(t)\|^2$$

[Zelazo 25]

SYMMETRY FORCED FORMATION CONTROL

The states can be defined as $\tilde{p}(t) = Pp(t) = \begin{bmatrix} p_0^T(t) & p_f^T(t) \end{bmatrix}^T$, for some permutation matrix P .

- $p_0(t)$ - the restriction of the configuration vector $p(t)$ to agents in the representative vertex set \mathcal{V}_0 .
- $p_f(t)$ - The remaining agents

Propose the gradient control

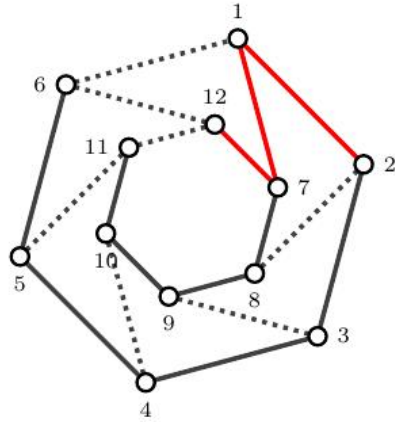
$$u(t) = -\nabla F_f(p(t))$$

The dynamics in state-space form become

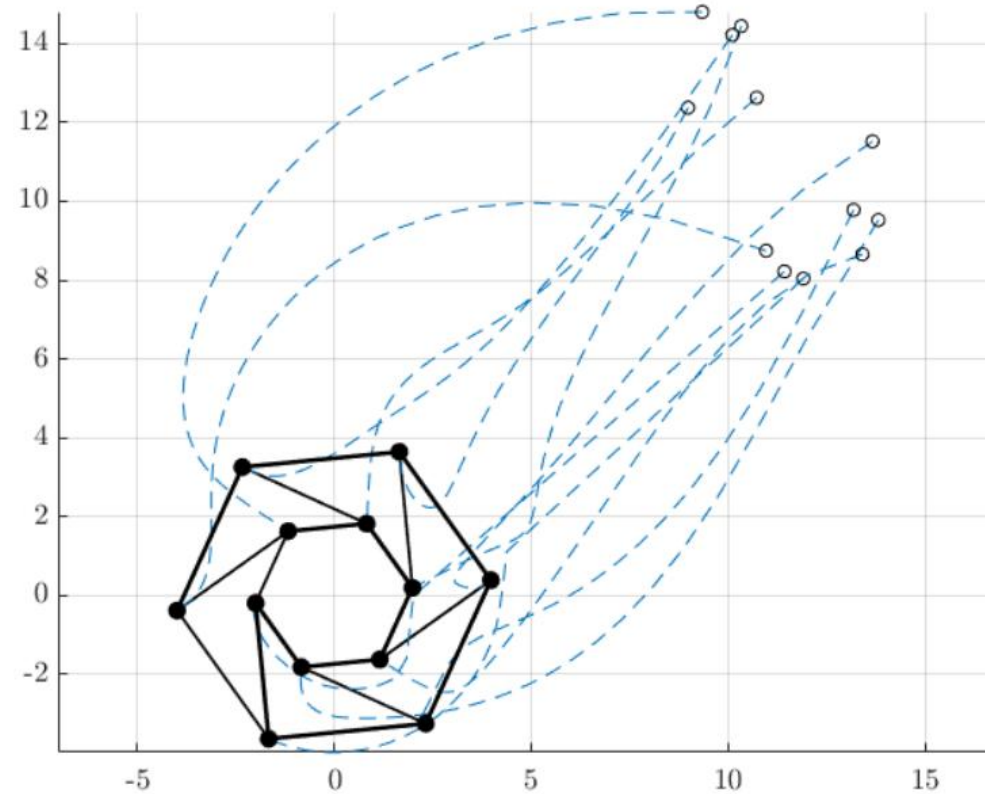
$$\begin{bmatrix} \dot{p}_0(t) \\ \dot{p}_f(t) \end{bmatrix} = \begin{bmatrix} -\mathcal{O}^T(\mathcal{G}_0, p_0(t)) \left(\mathcal{O}(\mathcal{G}_0, p_0(t)) p_0(t) - \mathbf{d}_0^2 \right) \\ 0 \end{bmatrix} - PQP^T \begin{bmatrix} p_0(t) \\ p_f(t) \end{bmatrix}$$

[Zelazo 25]

SYMMETRIC FORMATION - EXAMPLE



- $2\pi/6$ rotational symmetry
- Requires at least 21 edges for "classic" formation control
- Symmetry forced formation control requires only 11 edges



$\tau(\Gamma)$ -symmetric frameworks by definition have point-group symmetries defined with respect to some fixed inertial point.

Q: Can the formation acquisition problem be achieved while simultaneously moving the formation through space as a rigid body ?

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Q: Can the formation acquisition problem be achieved while simultaneously moving the formation through space as a rigid body ?

A: Yes! By implementing a virtual state $r(t) \in \mathbb{R}^d$ as the reference signal for the agents to arrange themselves with respect to any point.

SPECIAL CASE: FLOCKING

The trajectory consists only of a translation component, known by all agents.

Define the shifted state:

$$\bar{c}(t) = \begin{bmatrix} c_0^T(t) & c_f^T(t) \end{bmatrix}^T = P(p(t) - \mathbf{1} \otimes r(t))$$

choose $\begin{bmatrix} \dot{p}_0(t) & \dot{p}_f(t) \end{bmatrix}^T = u(t) = u_a(t) + u_m(t)$

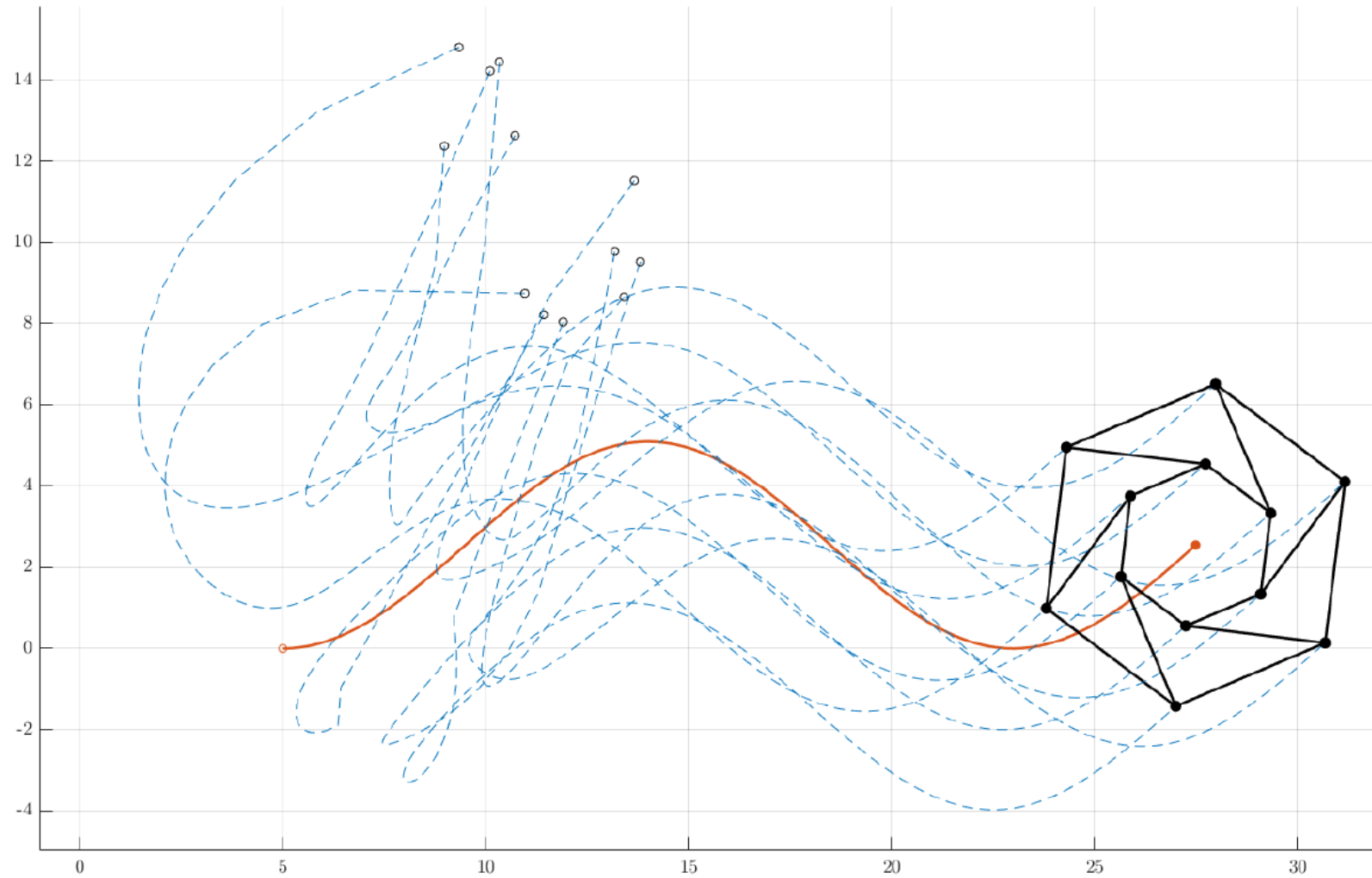
- **Formation Acquisition**

$$u_a(t) = \begin{bmatrix} -\mathcal{O}^T(\mathcal{G}_0, c_0(t)) \left(\mathcal{O}(\mathcal{G}_0, c_0(t)) c_0(t) - \mathbf{d}_0^2 \right) \\ 0 \end{bmatrix} - P Q P^T \begin{bmatrix} c_0(t) \\ c_f(t) \end{bmatrix}$$

- **Formation Maneuvering**

$$u_m(t) = \mathbf{1} \otimes \dot{r}(t)$$

FLOCKING - EXAMPLE



FLOCKING: DISTRIBUTED APPROACH

A single agent is subjected to the reference velocity input.

The modified control including a reference model takes the form:

$$\begin{bmatrix} \dot{p}_0(t) \\ \dot{p}_f(t) \end{bmatrix} = \begin{bmatrix} -\mathcal{O}^T(\mathcal{G}_0, c_0(t)) \left(\mathcal{O}(\mathcal{G}_0, c_0(t)) c_0(t) - \mathbf{d}_0^2 \right) \\ 0 \end{bmatrix} - P Q P^T \begin{bmatrix} c_0(t) \\ c_f(t) \end{bmatrix} + \dot{\bar{r}}(t)$$

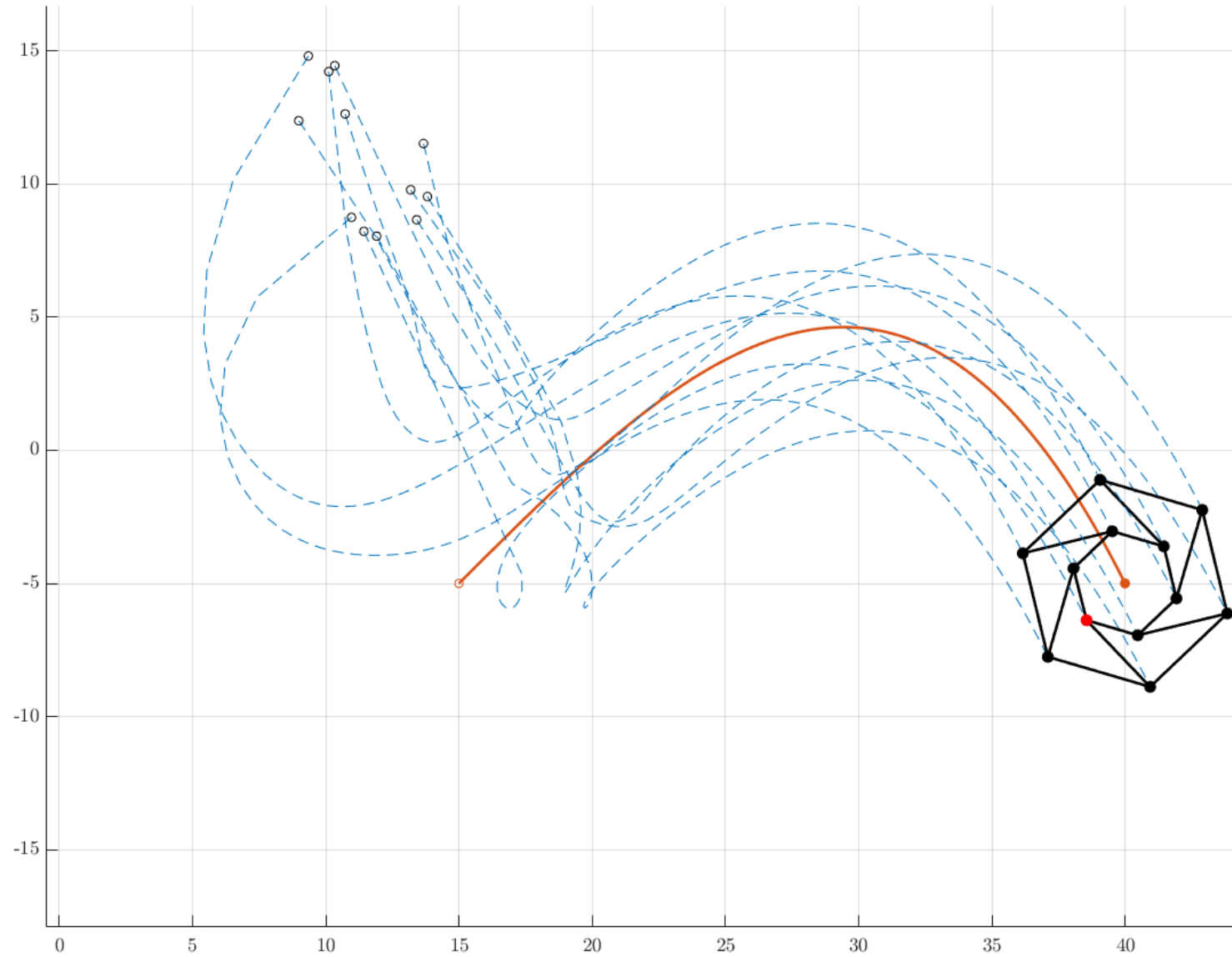
The trajectory is computed distributedly based to the consensus protocol:

$$\begin{cases} \dot{\bar{r}} &= -k_P \bar{L}(\mathcal{G}) \bar{r} - k_I \bar{L}(\mathcal{G}) \bar{\zeta} + n B \otimes v_0(t) \\ \dot{\bar{\zeta}} &= \bar{L}(\mathcal{G}) \bar{r} \end{cases}$$

where:

- $v_0 \in \mathbb{R}^d$ is the reference velocity input
- $B \in \mathbb{R}^n$ is a standard base vector denoting which agent is subjected to $v_0(t)$

FLOCKING: DISTRIBUTED APPROACH - EXAMPLE



SYMMETRY CONSTRAINED FORMATION MANEUVERING

Symmetry-constrained formations undergoing rotations requires time-varying point group symmetries

A similarity transformation of a point group element $\tau(\gamma)$ by a rotation matrix $R(\theta(t))$ reorients the isometries about $\theta(t)$ in the original frame

$$\tau(\gamma, \theta(t)) = R(\theta(t))\tau(\gamma)R(\theta(t))^{-1}$$

Notations:

- $\theta(t)$ - The orientation of the rigid body
- $\omega_0(t)$ - The desired angular velocity vector

SYMMETRY CONSTRAINED FORMATION MANEUVERING

Assumption: The centroid of the formation is defined at the origin

Recall the defined shifted state:

$$\bar{c}(t) = \begin{bmatrix} c_0^T(t) & c_f^T(t) \end{bmatrix}^T = P(p(t) - \mathbf{1} \otimes r(t))$$

choose $\begin{bmatrix} \dot{p}_0(t) & \dot{p}_f(t) \end{bmatrix}^T = u(t) = u_a(t) + u_m(t)$

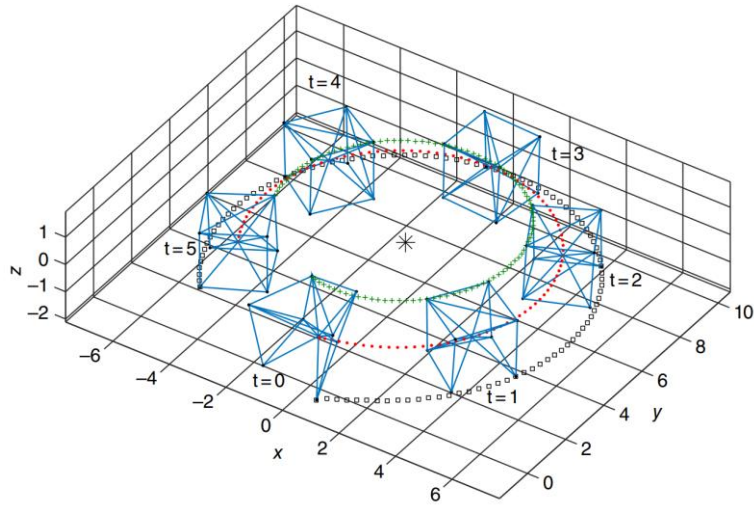
- **Formation Aquisition**

$$u_a(t) = \begin{bmatrix} -\mathcal{O}^T(\mathcal{G}_0, c_0(t), \tau(t)) \left(\mathcal{O}(\mathcal{G}_0, c_0(t), \tau(t)) c_0(t) - \mathbf{d}_0^2 \right) \\ 0 \end{bmatrix} - PQ(\tau(t))P^T \begin{bmatrix} c_0(t) \\ c_f(t) \end{bmatrix}$$

- **Formation Maneuvering**

$$u_m(t) = \mathbf{1} \otimes \dot{r}(t) + \begin{bmatrix} \vdots \\ \omega_0(t) \times p_i(t) \\ \vdots \end{bmatrix}$$

SYMMETRY CONSTRAINED FORMATION MANEUVERING - EXAMPLE

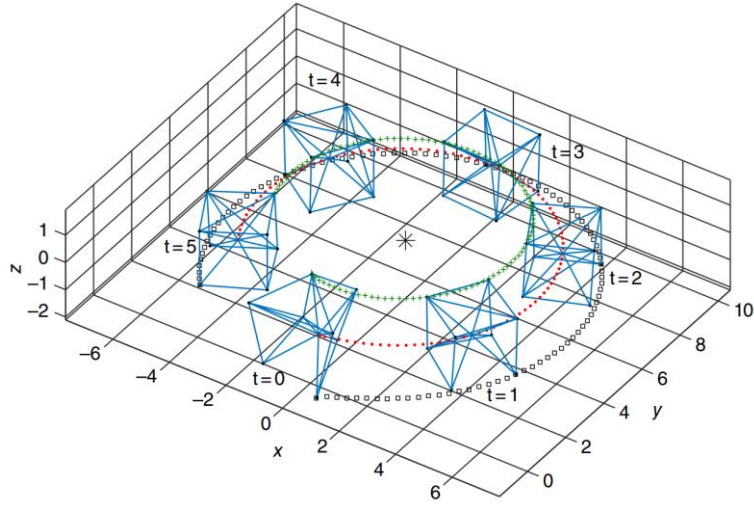


[Queiroz 18]

For classic formation control:

- A desired cube formation requires a known agent representing its geometric center
- At least 21 edges are required for infinitesimal rigidity

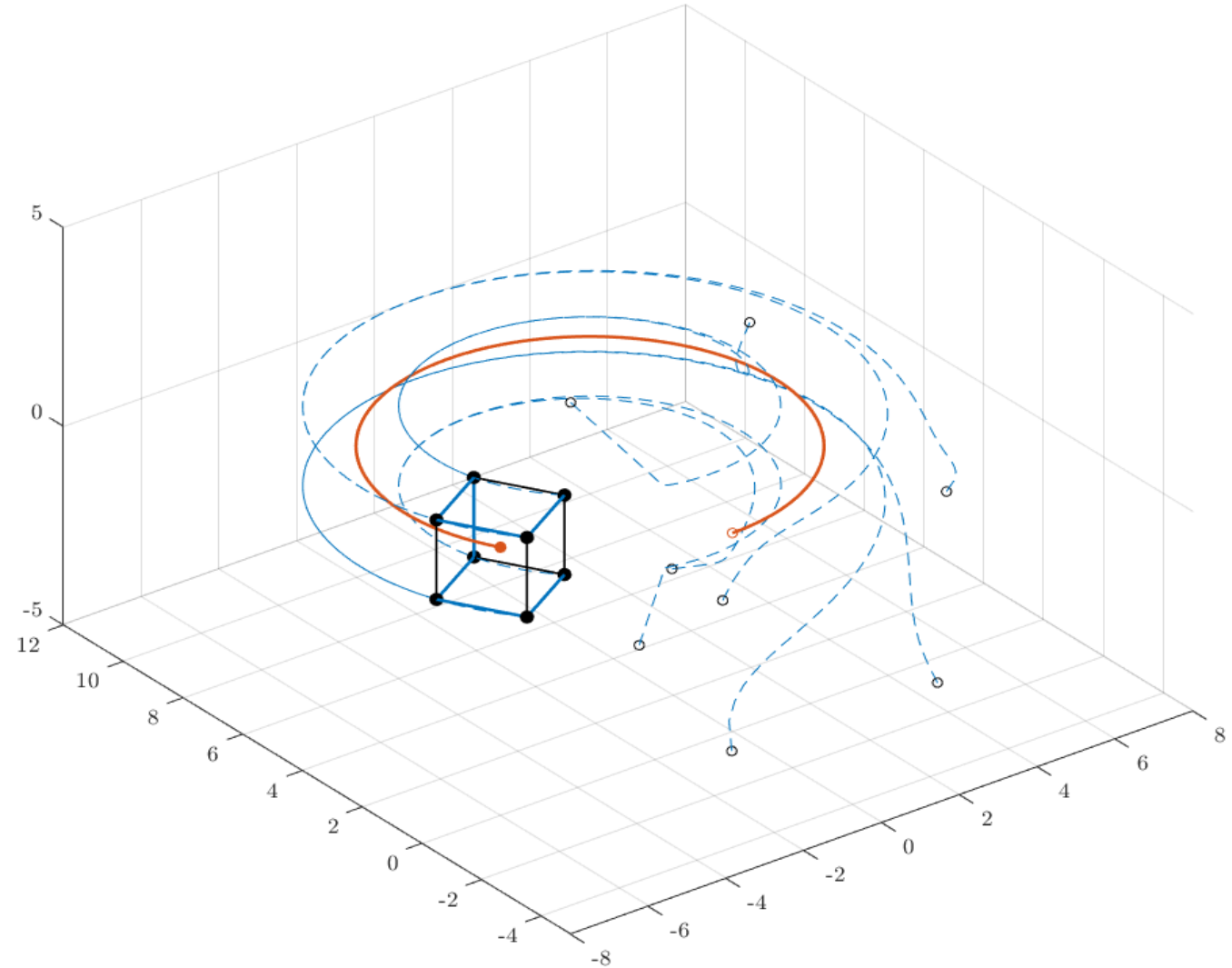
SYMMETRY CONSTRAINED FORMATION MANEUVERING - EXAMPLE



[Queiroz 18]

A symmetry constrained cube formation:

- has its geometric center at the origin
- requires 7 edges



Summary

- Symmetry-constrained formations require simpler graphs with significantly fewer information links compared to “classic” strategies
- The velocity reference command can be assigned to a single agent
- Point group symmetries can be conserved during rotations of the rigid body

Future Work

- Extending the approach to multi-agent systems with double integrator dynamics
- Exploring extensions for bearing rigidity

Questions?